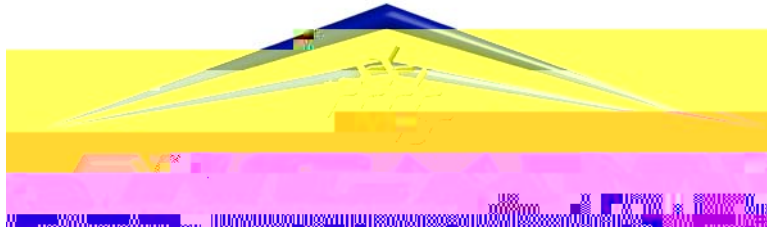


Report No: NCP-RP-2018-017 Rev N/C
Report Date: December 19, 2019"



Equivalency Statistical Analysis for Laminate Repair Prepreg Batch of Solvay (Formerly Cytec) 5320-1 T650 3K-PW fabric with 36% RC

NCAMP Project Number: NPN 031801

NCAMP Test Report Number: NCP-RP-2018-017 Rev N/C"

Report Date: December 19, 2019

Elizabeth Clarkson, Ph.D.

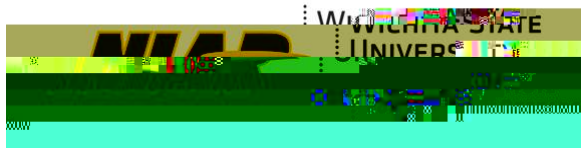
Pcvkqpcn"Egpgvt"hqt"Cfxcpgef"Ocvgtkcnu"Rgthqt o cpeg"*PECOR+
Pcvkqpcn"Kpukvwvg"hqt"Cxkcvkqp"Tgugcte.j"
Yke.jkvc"Uvcvg"Wpkxgtukv{"
Yke.jkvc."MU"89482/22;5"

Testing Facility:

Pcvkqpcn"Kpukvwvg"hqt"Cxkcvkqp"Tgugcte.j"
Yke.jkvc"Uvcvg"Wpkxgtukv{"
3:67"P0"Hckt o qwpv"
Yke.jkvc."MU"89482/22;5"
"

Test Panel Fabrication Facility:

Pcvkqpcn"Kpukvwvg"hqt"Cxkcvkqp"Tgugcte.j/PECV"
Yke.jkvc"Uvcvg"Wpkxgtukv{"



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Report Date: December 19, 2019"

Prepared by:

Elizabeth Clarkson

Reviewed by:

" **Jonathan Tisack**

Approved by:

" **Royal Lovingfoss** "

Nkuv"qh"Vcdngu"

Vcdng"3/3"Vguv"Rtqrgtv{"Cddtgxkcvkqpu"00"9
 Vcdng"3/4"Gpxktqp o gpvcn"Eqpfkvkqpu"Cddtgxkcvkqpu"00"9
 Vcdng"4/3"Qpg/ukfgf"vqngtcepeg"hcevqtu"hqt"nk o kvu"qp"uc o rng" o gcp"xcnwgwu"00"33
 Vcdng"4/4"Qpg/ukfgf"vqngtcepeg"hcevqtu"hqt"nk o kvu"qp"uc o rng" o kpk o w o "xcnwgwu"00"34
 Vcdng"5/3"Uw o oct{"qh"Gswkxcngpe{"Vguv"Tguwnvu"00"37
 Vcdng"5/4"\$ "Hckngf\$"Tguwnvu"Uecng"00"38
 Vcdng"5/5"Yctr"Eq o rtguukqp"Uvtgpi v j" Tguwnvu"00"3:
 Vcdng"5/6"Yctr"Eq o rtguukqp"Oqfwnwu" Tguwnvu"00"3:
 Vcdng"5/7"Yctr"Vgpukqp"Uvtgpi v j" Tguwnvu"00"42
 Vcdng"5/8"Yctr"Vgpukqp"Oqfwnwu" Tguwnvu"00"42
 Vcdng"5/9"Hknn"Eq o rtguukqp"Uvtgpi v j" Tguwnvu"00"44
 Vcdng"5/: "Hknn"Eq o rtguukqp"Oqfwnwu" Tguwnvu"00"44
 Vcdng"5/;"Hknn"Vgpukqp"Uvtgpi v j" Tguwnvu"00"46
 Vcdng"5/32"Hknn"Vgpukqp"Oqfwnwu" Tguwnvu"/

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1. Introduction

rgthqtokpi"rgtkqfke"gswkxcngpe{lcf flvkqpcn"vguvki."rctvkekrcvki"kp"ocvgtkcn"ejcpig"opcigogpv"
cevxkvkgu."eqpfwevki"uvckvkecn"rtqeguu"eqpvtqn."cpf"eqpfwevki"tgiwnct"uwrrnktg"cwfkvu0"

Vjg"crnkcdknkv{"cpf"ceewtce{"qh"PECOR"ocvgtkcn"rtqrgtv{"fcvc."ocvgtkcn"cnnycdngu."cpf"
urgekhkecvkqpu"owuv"dg"gxcnwcvgf"qp"ecug/d{/ecug"dcuku"d{"cktetchv"eqorcpkgu"cpf"egtvkh{kpi"
cigpekgu0"PECOR"cuuwogu"pq"nkcdknkv{"yjcvuqgxtg."gzrtguugf"qt"korngkf."tgnvcvgf"vq"vjg"wg"qh"
vjg"ocvgtkcn"rtqrgtv{"fcvc."ocvgtkcn"cnnycdngu"cpf"urgekhkecvkqpu0"

Vjg"fcvc"kp"vjku"tgrqtv"ku"kpvgpfgf"hq"igpgtcn"fkuvtkdvwkqp"vq"vjg"rwdnke."gkvjgt"htgg{"qt"cv"c"rtkeg"
vjcv"fqgu"pqv"gzeggf"vjg"equv"qh"tgrtqfwevki"gi0"rtkpvki+"cpf"fkuvtkdvwkqp"gi0"rquvcig+0"

1.1 Symbols and Abbreviations

Test Property	Abbreviation
Yctr"Eqo rtguukqp"	YE"
Yctr"Vgpukqp"	YV"
Hknn"Eqo rtguukqp"	HE"
Hknn"Vgpukqp"	HV"
Kp/Rncpg"Ujgct"	KRU"
Ujqtv"Dgco"Uvtgpi vj"	UDU"
Qrgp"Jqng"Vgpukqp"	QJV"
Qrgp"Jqng"Eqo rtguukqp"	QJE"
Eqo rtguukqp"Chvgt"Korcev"	ECK"
Ewtgfrn{"Vjkempguu"	ERV"
F{pcke"Ogejcpkecn"Cpcn{uku	FOC"

Table 1-1 Test Property Abbreviations

Environmental Condition	Temperature	Abbreviation
Eqnf"Vgorgtcvwtg"ft{"	87a07•H"	EVF"
Tqqo"Vgorgtcvwtg"ft{"	97a032•H"	TVF"
Gngxcvgf"Vgorgtcvwtg"Ygv"	472a07•H"	GVY4"

Table 1-2 Environmental Conditions Abbreviations

Vguvu"ykvj"cpwodgt"koogfkcygn{"chvgt"vjg"cdtdgxkcvkqp"kpfkcevg"vjg"nc{/wr<
"
"
3"tghgtv"vq"47172147"nc{wr0"Vjku"ku"cnuq"tghgttgf"vq"cu"õSwcuk/Kuqvtqrke0"
4"tghgtv"vq"321:2132"nc{wr0"Vjku"ku"cnuq"tghgttgf"vq"cu"õUqhv0"
5"tghgtv"vq"62142162"nc{wr0"Vjku"ku"cnuq"tghgttgf"vq"cu"õJctf0"
"
"
GZ<"QJV3"ku"cp"qrgp"jqng"vgpukqp"vguv"ykvj"swcuk/kuqvtqrke"nc{wr0"

2. Background

Gswkxcngpeg"vguvu"ctg"rgthqt o gf"kp"ceeqtfcpeg"ykvj"ugevkqp":0603"qh"EO J/39/3 I"cpf"ugevkqp"803"
 qh"FQVIHCCICT/2513;.δOcvgtkcn"Swcnkhkecvkqp"cpf"Gswkxcngpe{"hqt"Rqn{ o gt"Ocvtkz"
 Eq o rqukvg"Ocvgtkcn"U{ uvg o uκ"W r fcvgf"Rtqegfwtgöö"
 "

2.1 Results Codes

Pass"kpfkcevgu"vjcv"vjg"vguv"tguwnvu"ctg"gswwxcngpv"hqt"vjcv"gpvktqp o gpv"wpfgt"dqvj"eq o rwwcvkqpcn"
 o gvjqfu0"
 "

Fail"kpfkcevgu"vjcv"vjg"vguv"tguwnvu"ctg"PQV"gswwxcngpv"wpfgt"dqvj"eq o rwwcvkqpcn" o gvjqfu0"
 "

Pass with Mod CV kpfkcevgu"vjg"vguv"tguwnvu"ctg"gswwxcngpv"wpfgt"vjg"cuuw o rvkqp"qh"vjg" o qfkhkgf"
 EX" o gvjqf"vjcv"vjg"eqghkekgpv"qh"xctkcvkqp"ku"cv"ngcuv"8"dww"vjg"vguv"tguwnvu"hc kn"ykvjqwv"vjg"wg"qh"
 vjg" o qfkhkgf"EX" o gvjqf0"
 "

2.2 Equivalency Computations

Gswkxcngpe{"vguvu"ctg"rgthqt o gf"vq"fgvgt o kpg"kh"vjg"fkhhgtgpegu"dgvyggp"vguv"tguwnvu"ecp"dg"
 tgcupcdn{"gzrnckpgf"cu"fwg"vq"vjg"gzrgevfg"tcpfq o "xctkcvkqp"qh"vjg" o cvgtkcn"cpf"vguvkpi"
 rtqeguugu0"Kh"uq."y g"ecp"eqpenwfg"vjg"v y q"ugvu"qh"vguvu"ctg"htq o "-:gswkxcngpvø" o cvgtkcnu0"
 "

2.2.1 Hypothesis Testing

Vjku"eq o rctkuqp"ku"rgthqt o gf"wukpi"vjg"uvcvkuvkecn" o gvjqfqni {"qh"j { rqvjguku" 6 Z go

2.2.2 Type I and Type II Errors

	<i>Materials are equal</i>	<i>Materials are not equal</i>
--	--------------------------------	--

*Conclude
materials
are equal*

Correct

2.2.4 Strength and Modulus Tests

Hqt"uvtgpi vj "vguv"xcnwgu." yg"ctg" rtk o ctkn{ "eqpegtpgf" qpn{ "kh"vjg"gswxncngpeg"uc o rng"ujqyu"nqygt"
 uvtgpi vj "xcnwgu"vjcp"vjg"qtkikpcn"swcnkhkecvkqp" o cvgtkcno"Vjku"ku"tghgttgf"vq"cu"c"qpg/ukfgf0"
 j { rqvjguku"vguv0" Jki jgt"xcnwgu"ctg"pqv"eqpukfgtgf"c"rtqdn go ."vjqwi j"vjg{ "oc{ "kpfkecvg"c"
 fkhhtgpeg"dgvyggp"vjg"vyq" o cvgtkcno"Vjg"gswxncngpeg"uc o rng" o gcp"cpf"uc o rng" o kpk o w o "
 xcnwgu"ctg"eq o rctgf"ci ckpuv"vjg" o kpk o w o "gzrgevfg"xcnwgu"hqt"vjqug"ucvkuvkeu." y jkej"ctg"
 eq o rwwgf"htq o "vjg"swcnkhkecvkqp"vguv"tguwnv0"
 "

Vjg"gzrgevfg"xcnwgu"ctg"eq o rwwgf" wukpi "vjg"xcnwgu"nkuvfg"kp"Vcdng"4/3"cpf"Vcdng"4/4"ceeqtfkpi "
 vq"vjg"hqnnqykpi "hqt o wncu<"
 "

$$Vjg" o gcp" o wuv"gzeggf" \bar{X} \quad k_n^{table 403} \quad S \quad y jgtg" \bar{X} \quad cpf"U"ctg."tgur gev kxgn\{."vjg" o gcp"cpf"vjg" \\
 uvcpfctf" fgxkcvkqp"qh"vjg"swcnkhkecvkqp"uc o rng0""$$

$$Vjg"uc o rng" o kpk o w o " o wuv"gzeggf" \bar{X} \quad k_n^{table 404} \quad S \quad y jgtg" \bar{X} \quad "cpf"U"ctg."tgur gev kxgn\{."vjg" \\
 o gcp"cpf"vjg"uvcpfctf" fgxkcvkqp"qh"vjg"swcnkhkecvkqp"uc o rng0""$$

Kh"gvjgt"vjg" o gcp"qt"vjg" o kpk o w o "hcnu"dgnqy"vjg" _

	0.25	0.1	0.05	0.025	0.01	0.005	0.0025	0.001	0.0005
2	0.6266	1.0539	1.3076	1.5266	1.7804	1.9528	2.1123	2.3076	2.4457
3	0.5421	0.8836	1.0868	1.2626	1.4666	1.6054	1.7341	1.8919	2.0035
4	0.4818	0.7744	0.9486	1.0995	1.2747	1.3941	1.5049	1.6408	1.7371
5	0.4382	0.6978	0.8525	0.9866	1.1425	1.2488	1.3475	1.4687	1.5546
6	0.4048	0.6403	0.7808	0.9026	1.0443	1.1411	1.2309	1.3413	1.4196
7	0.3782	0.5951	0.7246	0.8369	0.9678	1.0571	1.1401	1.2422	1.3145
8	0.3563	0.5583	0.6790	0.7838	0.9059	0.9893	1.0668	1.1622	1.2298
9	0.3379	0.5276	0.6411	0.7396	0.8545	0.9330	1.0061	1.0959	1.1596
10	0.3221	0.5016	0.6089	0.7022	0.8110	0.8854	0.9546	1.0397	1.1002
11	0.3084	0.4790	0.5811	0.6699	0.7735	0.8444	0.9103	0.9914	1.0490
12	0.2964	0.4593	0.5569	0.6417	0.7408	0.8086	0.8717	0.9493	1.0044
13	0.2856	0.4418	0.5354	0.6168	0.7119	0.7770	0.8376	0.9121	0.9651
14	0.2760	0.4262	0.5162	0.5946	0.6861	0.7488	0.8072	0.8790	0.9300
15	0.2673	0.4121	0.4990	0.5746	0.6630	0.7235	0.7798	0.8492	0.8985
16	0.2594	0.3994	0.4834	0.5565	0.6420	0.7006	0.7551	0.8223	0.8700
17	0.2522	0.3878	0.4692	0.5400	0.6230	0.6797	0.7326	0.7977	0.8440
18	0.2455	0.3771	0.4561	0.5250	0.6055	0.6606	0.7120	0.7753	0.8202
19	0.2394	0.3673	0.4441	0.5111	0.5894	0.6431	0.6930	0.7546	0.7984
20	0.2337	0.3582	0.4330	0.4982	0.5745	0.6268	0.6755	0.7355	0.7782
21	0.2284	0.3498	0.4227	0.4863	0.5607	0.6117	0.6593	0.7178	0.7594
22	0.2235	0.3419	0.4131	0.4752	0.5479	0.5977	0.6441	0.7013	0.7420
23	0.2188	0.3345	0.4041	0.4648	0.5359	0.5846	0.6300	0.6859	0.7257
24	0.2145	0.3276	0.3957	977	7				

	0.25	0.1	0.05	0.025	0.01	0.005	0.0025	0.001	0.0005
2	1.2887	1.8167	2.1385	2.4208	2.7526	2.9805	3.1930	3.4549	3.6412
3	1.5407	2.0249	2.3239	2.5888	2.9027	3.1198	3.3232	3.5751	3.7550
4	1.6972	2.1561	2.4420	2.6965	2.9997	3.2103	3.4082	3.6541	3.8301
5									

"
 V jku"ku"eqpxgtvgf"vq"rgtegpv"d{" o wnvkrn{kpi"d{"322 ' 0"
 " EX"ku"wugf"vq"eq o rrwg"c" o qfkhkgf"uvcpfctf"fgxkcvkqp"U·0"
 "

$$S = CV \cdot \bar{X} \tag{Equation 2}$$

"
 Vq"eq o rrwg"vjg"rqqngf"uvcpfctf"fgxkcvkqp"dcugf"qp"vjg" o qfkhkgf"EX<"
 "

$$S_p = \sqrt{\frac{\sum_{i=1}^k n_i (CV_i - \bar{X}_i)^2}{k-1}} \tag{Equation 3}$$

"
 Vjg"C/dcuku"cpf"D/dcuku"xcnwgu"wpfgt"vjg"cuuw o rvkqp"qh"vjg" o qfkhkgf"EX" o gvjqf"ctg"eq o rrwg"
 d{"tgrncekpi"U" ykvj"U·0"
 "

Y jgp"vjg"dcuku"xcnwgu" jcxg"dggp"ugv"wukpi"vjg" o qfkhkgf"EX" o gvjqf." yg"ecp"wug"vjg" o qfkhkgf"
 EX"vq"eq o rrwg"vjg"gswkxcngpe{"vguv"tguwnvu0"
 "

3. Equivalency Test Results

Vjgtg"ygtg"cvqvcn"qh"5;"fkhhtgtpv"vguvu"qh"gswxncngpeg"twp"ykvj"uwhhkekppv"fcvc"ceeqtfkpi"vq"vjg"
 tgeqo"ogpfcvkqpu"qh"EOJ/39/3I0"Vjgtg"ygtg"cp"cfkvwkqpcn"vyq"vguvu"rgthqtogf"ykvj"
 kpuwhhkekppv"fcvc0"C"eqo"rectkuqp"qh"vjg"cxgtcig"ewtgf"rn{"vj" Kempguu"cpf"FOC"tguwnvu"ycu"cnuc"
 ocfg0"Cnn"vguvu"ygtg"rgthqtogf"ykvj"cp" "ngxgn"qh"7 ' 0"

Vjg"tguwnvu"qh"vjg"gswxncngpe{"eqo"rectkuqp"ctg"nkuvgf"cu":Rcuuø."÷Hcknø."qt":Rcuu"ykvj"Oqf"EXø0"
 :Rcuu"ykvj"Oqf"EXø"tghgtu"vq"ecugu"y"jgtg"vjg"gswxncngpe{"hcknu"wpnguu"vjg"oqfkhkgf"eqghhkekppv"
 qh"xctkcvkqp"ogvjqf"ku"wugf0"C"okpkowo"qh"gkijv"uc"o"rngu"htqo"vyq"ugrctcvg"rcpgnu"cpf"
 rtqeguukpi"e{engu"ku"tgswtgf"htq

"

Description	Modulus	Strength
Oknf"Hcknwtg"	' "hckn""Ö"6 ' "	' "hckn""Ö"7 ' "
Oknf"vq"Oqfgtcvg"Hcknwtg"	6 ' ">" ' "hckn""Ö": ' "	7 ' ">" ' "hckn""Ö"32 ' "
Oqfgtcvg"Hcknwtg"	: ' ">" ' "hckn""Ö"34 ' "	32 ' ">" ' "hckn""Ö"37 ' "
Oqfgtcvg"vq"Ugxgtg"Hcknwtg"	34 ' ">" ' "hckn""Ö"38 ' "	37 ' ">" ' "hckn""Ö"42 ' "
Ugxgtg"Hcknwtg"	38 ' ">" ' "hckn""Ö"42 ' "	42 ' ">" ' "hckn""Ö"47 ' "
Gzvtg o g"Hcknwtg"	42 ' ">" ' "hckn"	47 ' ">" ' "hckn"

Table 3-2 "% Failed" Results Scale

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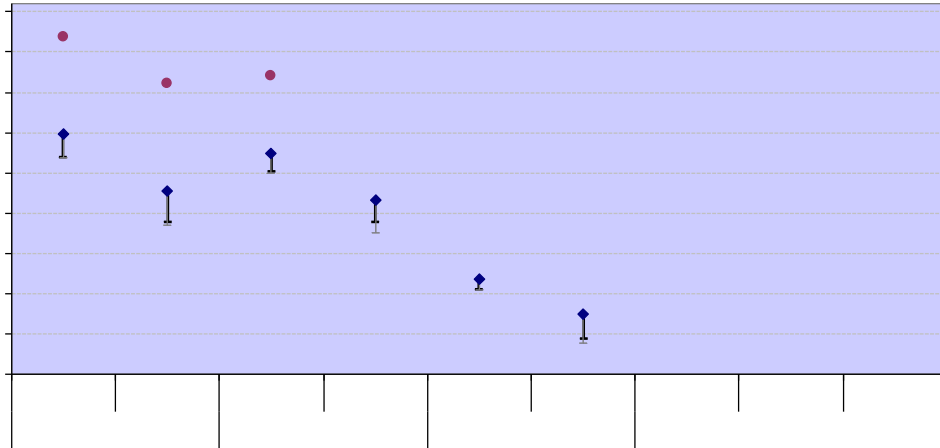
I tcr jkecn"rtgugpvcvkqpu"qh"cm"vg

3.1 Warp Compression (WC)

Vjg"YE"fcvc"ku"pqt o cnk |gf0"Dqvj"vjg"YE"uvtgpi vj"fcvc"cpf" o qfwnwu"fcvc"rcuugf"gswxengpe{"
 vguvu"hqt"cn"vguvgf"eqpfkvkqpu0""Uvcvkuvkeu"cpf"cpn{uku"tguwnvu"ctg"ujqyp"hqt"vjg"uvtgpi vj"fcvc"kp"
 Vcdng"5/5"cpf"hqt"vjg" o qfwnwu"fcvc"kp"Vcdng"5/60"

	Qual.	Equiv.	Qual.	Equiv.	Qual.	Equiv.
Fcvc"pqtocnk gf"ykvj"ERV"202299						
Ogcp"Uvtgpi vj"*muk+	32906:7	3530847	3240897	3440385	930633	990329
Uvepctf"fgxkcvkqp	:0253	7024:	80484	50:77	60:75	8058:

Hkiwtg"5/5"knwuvtcvgu"vjg"2à"Eqo rtguukqp"uvtgpi vj " ogcpu"cpf" okpkow o "xcnwgucpf" oqfwnwu"
ogcpu"hqt"vjg"swcnkhkecvkqp"uc o rng"cpf"vjg"gswxengpe{"uc o rng0"Vjg"nko kvu"hqt"gswxengpe{"
uc o rngu"ctg"ujqyp"cu"gttqt"dctu"ykvj"vjg"swcnkhkecvkqp"fcvc0"Vjg"nqpi gt."nki jvgt"eqnqtgf"gttqt"dctu"
ctg"hqt"vjg"oqfkhkgf"EX"eqo rwvcvkqpu0"
"



3.2 Warp Tension (WT)

Vjg"YV"fcvc"ku"pqt ocnk|gf0"Dqvj"vjg"YV"vgtgpi vj"fcvc"cpf"o qfwnwu"fcvc"rcuugf"gswxengpe {"
 vguvu"hqt"cn"vguvgf"eqpfkvkqpu0"Uvcvkuvkeu"cpf"cpn{uku"tguwnvu"ctg"ujqyp"hqt"vjg"vgtgpi vj"fcvc"kp"
 Vcdng"5/7"cpf"hqt"vjg"o qfwnwu"fcvc"kp"Vcdng"5/80"
 "

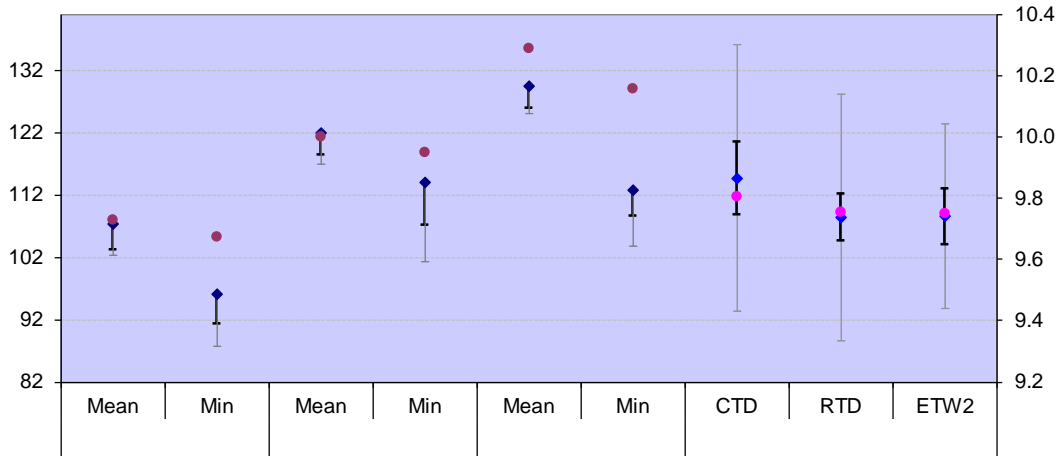
Warp Tension (WT) Strength	CTD		RTD		ETW2	
	Qual.	Equiv.	Qual.	Equiv.	Qual.	Equiv.
Fvc"pqtocnk gf"ykvj"ERV"2/2299						
Ogcp"Uvgtgpi vj"*muk+	329/49;	32:0243	3430:5:	3430/538	34:0576	3570/632
Uvcpfctf"fgxkcvkqp	70:;6	40622	70547	40238	90297	5056;
Eqghhkekgpv"qh"Xctkcvkqp"'	706;6	40444	60593	30884	7068;	40695
Olpkwo	;70;5	3270395	3350;43	33:0:2:	3340:36	34:025:
Oczkwo	3430/276	333099;	3530/827	346088;	3590778	362075:
Pwodgt"qh"Urgekogpu	43	:	44	:	44	38
RESULTS	PASS		PASS		PASS	
Olpkwo"Ceegrvcvng"Gswx0/Ucoring"Ogcp	3250499		33:0646		3470:56	
Olpkwo"Ceegrvcvng"Gswx0/Ucoring"Olp	;30587		3290464		32:082;	
MOD CV RESULTS	PASS with MOD CV		PASS with MOD CV		PASS with MOD CV	
Oqfhhkgf"EX"'	80969		803:7		80957	
Olpkwo"Ceegrvcvng"Gswx0/Ucoring"Ogcp	3240586		3390229		3470365	
Olpkwo"Ceegrvcvng"Gswx0/Ucoring"Olp	:90958		32303:3		3250:2;	

Table 3-5 Warp Tension Strength Results

"

	Qual.	Equiv.	Qual.	Equiv.	Qual.	Equiv.
Fvc"pqtocnk gf"ykvj"ERV"2/2299						
Ogcp"Oqfwnwu"*Ouk+	;0:87	;0:28	;095:	;0977	;0963	;0973
Uvcpfctf"fgxkcvkqp	2037:	20284	20326	20289	2035:	20367
Eqghhkekgpv"qh"Xctkcvkqp"'	30828	20859	30287	208::	30654	306:5
Olpkwo	;0773	;094:	;0769	;0885	;06;;	;06:9
Oczkwo	320285	;0:2:	;0:88	;0:24	;0:;9:0	09
E 30		50 è	lk o	e		

Hk i wtg"5/6"knwuvtcvgu"vjg"2à"Vgpukqp"uvtgpi vj " o gcpu"cpf" o kpk o w o "xcnwgu"cpf" o qfwnwu" o gcpu"hqt"
vjg"swcnkhkecvkqp"uc o rng"cpf"vjg"gswxengpe{"uc o rng"Vjg"nk o kvu"hqt"gswxengpe{"uc o rngu"ctg"
ujqyp"cu"gttqt"dctu"ykvj"vjg"swcnkhkecvkqp"fcvc"Vjg"nqpi gt."nki jvgt"eqnqtgf"gttqt"dctu"ctg"hqt"vjg"
o qfkhkgf"EX"eq o rwwcvkqpu0"
"

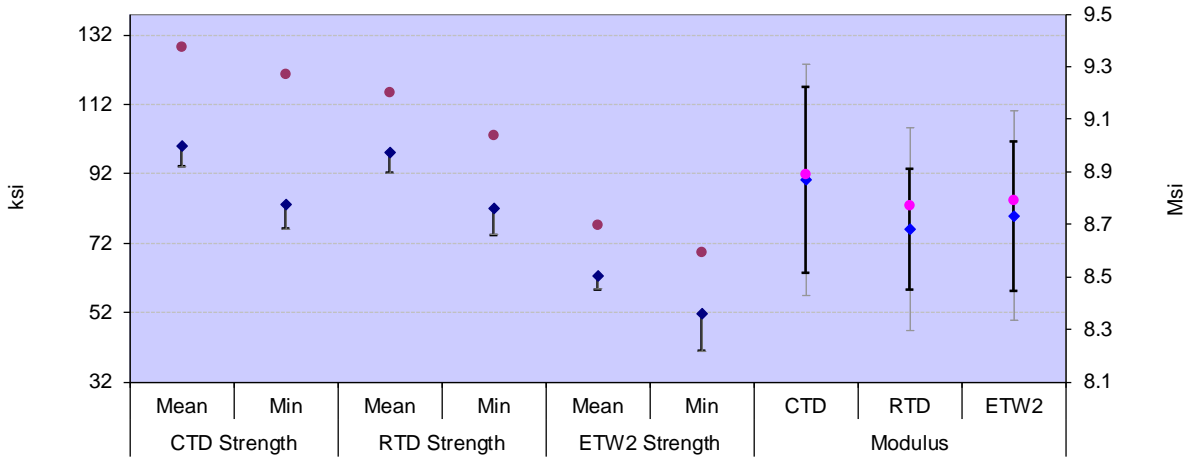


3.3 Fill Compression (FC)

Vjg"HE"fcvc"ku"pqt o cnk | gf0"Vjg"pqt o cnk | gf"HE"uvtgpi vj "fcvc"cpf" o qfwnwu"fcvc"rcuugf"
gswkxcngpe{ "vguvu"hqt"cnm"vguvvf"eqpfkvpqpu0""Oqfkhkgf"EX"tguwnvu"ygtg"pqv"rtqxkfgf"hqt"vjg"
uvtgpi vj "fcvc"dgecwug"vjg"eqghhkekgpv"qh"xctkcvkqp"ycu"cdqyg": '

Hkiwtg"5/7"knwuvtcvgu"vjg";2Å"Eqo rtguukqp"uvtgpi vj" ogcpu"cpf" o kpkow o "xcnwgucpf" o qfwnwu" o gcpu"hqt"vjg"swcnkhkecvkqp"uc o rng"cpf"vjg"gs wxcngpe {"uc o rng0"Vjg"nk o kvu"hqt"gs wxcngpe {" uc o rngu"ctg"ujqyp"cu"gttqt"dtu"ykvj"vjg"swcnkhkecvkqp"fcvc0"Vjg"nqpi gt."nki jvgt"eqnqtgf"gttqt"dtu" ctg"hqt"vjg" o qfkhkgf"EX"eq o r wvcvkqpu0"

Solvay (Formerly Cytec) 5320-1 T650 3k-PW fabric with 36% RC
 Comparison of FAA Laminate Repair Stud A 6 ir dA 2



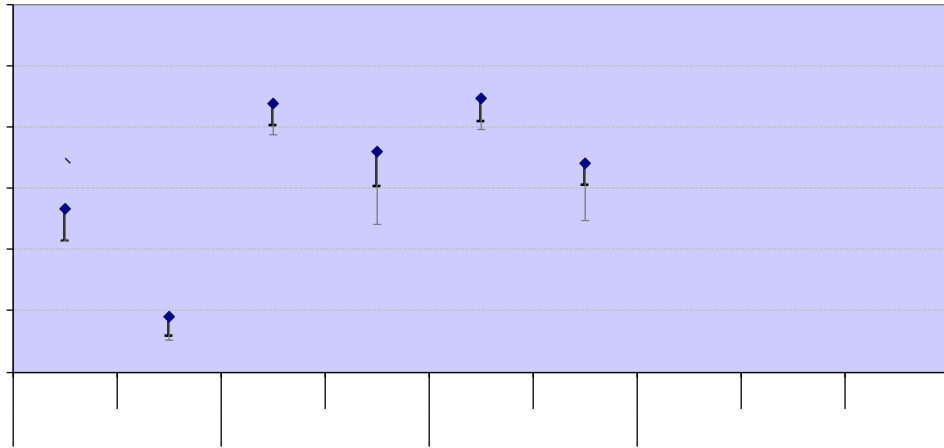
3.4 Fill Tension (FT)

Vjg"HV"fcvc"ku"pqt o cnk |gf0"Vjg"pqt o cnk |gf"HV"uvtgpi vj "fcvc"cpf" o qfwnwu"fcvc"rcuugf"
 gswkxcngpe{ "vguvu"hqt"cnm"vguvgf"eqpfkvkqpu0""

Uvcvkuvkeu"cpf"cpen{ uku"tguwnvu"ctg"ujqyp"hqt"vjg"uvtgpi vj "fcvc"kp"Vcdng"5/;"cpf"hqt"vjg" o qfwnwu"
 fcvc"kp"Vcdng"5/320"

Fill Tension (FT) Strength	CTD		RTD		ETW2	
	Qual.	Equiv.	Qual.	Equiv.	Qual.	Equiv.
Fcvc"pqtocnk gf"ykvj"ERV"2/2299						
Ogcp"Uvtgpi vj"*muk	323/7:4	326/44:	33:089:	337/796	33:0748	34:07:4
Uvcpfctf"Fgxkcvkqp	9/869	40:82	6/9;	5/9:8	7/385	6/755
Eqghhkeigpv"qh"Xctkcvkqp"'	9/749	4/966	6/3:8	5/498	6/542	5/6:;
Olpkwo	:5/;78	322/333	332/;2	332/288	32:0;5;	347/334
Oczkwo	337/3:6	32:044;	349/553	343/;77	348/858	358/722
Pwodgt"qh"Urgekogpu	43	:	43	:	43	:
RESULTS	PASS		PASS		PASS	
Olpkwo"Ceegrvcndng"Gswkx/0"Ucoring"Ogcp	:8/5; ;		337/4:9		338/242	
Olpkwo"Ceegrvcndng"Gswkx/0"Ucoring"Olp	:2/;66		327/456		327/7:8	
MOD CV RESULTS	PASS with MOD CV		PASS with MOD CV		PASS with MOD CV	
Oqfkhkgf"EX"'	9/986		8/2:;		8/382	
Olpkwo"Ceegrvcndng"Gswkx/0"Ucoring"Ogcp	:8/458		335/986		336/749	
Olpkwo"Ceegrvcndng"Gswkx/0"Ucoring"Olp	:2/4:8		;:035;		;:0869	

Hki wtg"5/8"knwuvtcvgu"vjg";2Å"Vgpukqp"uvtgpi vj" o gcpu"cpf" o kpkow o "xcnwgu"cpf" o qfwnwu" o gcpu"
hqt"vjg"swcnkhkecvkqp"uc o rng"cpf"vjg"gswxengpe{"uc o rng0"Vjg"nk o kvu"hqt"gswxengpe{"uc o rngu"ctg"
ujqyp"cu"gttqt"dctu"ykvj"vjg"swcnkhkecvkqp"fcvc0"Vjg"nqpi gt."nki jvgt"eqnqtgf"gttqt"dctu"ctg"hqt"vjg"
o fkhkgf"EX"eq o rwvcvkpu0"



3.5 Lamina Short Beam Strength (SBS)

Vjg"UDU"fcvc"ku"pqv"pqt o cnk | g f0"Vjg"UDU"fcvc"rcuugf"gs wxxcngpe {"vguvu"hqt"cn"vguvgf"eqp fkvkqpu0"

3.6 In-Plane Shear (IPS)

Vjg"KRU"fcvc"ku"pqv"pqt o cnk | gf0"Vjg"KRU"fcvc"rcuugf"cnm"gswxengpe{"vguvu"hqt"vjg"EVF"cpf"TVF"eqpfkvkqpu."cnvjqwij"vjg"uvtgpi vj"cv"7 " "uvtckp"fcvc"kp"vjg"EVF"eqpfkvkqp"tgswtgfvjg"wug"qh"vjg"o qfkhkgf"EX"cr rtqcej"vq"rcuu"gswxengpe{0"Vjg"KRU"fcvc"kp"vjg"GVY4"eqpfkvkqp"rcuugf"gswxengpe{"vguvu"qpn{"hqt"uvtgpi vj"cv"7 " "uvtckp."pqv"hqt"204 ' "qhhuvg"uvtgpi vj"qt"o qfwnwu0"Vjg"uvtgpi vj"cv"7 " "uvtckp"fcvc"kp"vjg"EVF"eqpfkvkqp"jcf"kp"uwhhkekgpv"fcvc"uvtgpi vj"tguwnv"vq"dg"eqpukfgtgf"eqpenwukxg0"

Uvcvkukcu"cpf"cpn{uku"tguwnvu"ctg"ujqyp"uvtgpi vj"204 ' "qhhuvg"uvtgpi vj"fcvc"kp"Vcdng"5/34."vjg"uvtgpi vj"cv"7 " "uvtckp"fcvc"kp"Vcdng"5/35."cpf"vjg"o qfwnwu"fcvc"kp"Vcdng"5/360"

In-Plane Shear (IPS) 0.2% Offset Strength	CTD		RTD		ETW2	
	Qual.	Equiv.	Qual.	Equiv.	Qual.	Equiv.
Fcvc"cu"ogcuwtgf						
Ogcp"Uvtgpi vj" B"204 ' "qhhuvg"*muk-	330726	330758	:04; ;	:0544	50982	50745
Uvcpfctf"fgxkcvkqp	2039;	203; 8	20356	20274	2037;	20288
Eqghhkekgpv"qh"Xctkcvkqp" ' "	3077;	30925	30834	20852	6045;	30: 92
Olpkow o	330233	33038;	:02; 7	:0452	50767	50656
Oczkow o	330: 78	3309: :	:0836	:0637	6032:	50855
Pwodgt"qh"Urgekogpu	43	32	43	:	43	:
RESULTS	PASS		PASS		FAIL	
Olpkow o"Ceegrvc dng"Gs wx0"Uc o r ng"O gcp	3305; 7		:042;		50874	
Olpkow o"Ceegrvc dng"Gs wx0"Uc o r ng"O lp	330228		90; 5:		50552	
MOD CV RESULTS	PASS with MOD CV		PASS with MOD CV		FAIL	
O q f khkg f"EX" ' "	80222		80222		8033;	
Olpkow o"Ceegrvc dng"Gs wx0"Uc o r ng"O gcp	3302: 6		90; 83		50826	
Olpkow o"Ceegrvc dng"Gs wx0"Uc o r ng"O lp	:07: 9		80; 77		5035;	

Table 3-12 In-Plane Shear 0.2% Offset Strength Results

In-Pl x

	Qual.	Equiv.	Qual.	Equiv.	Qual.	Equiv.
Fcvc"cu"ogcuwtgf	Insufficient Data					
Ogcp"Uvtgpi vj" B"7 ' "Uvtckp"*muk-	3:0: :4	3:052:	360872	360677	80; 37	80934
Uvcpfctf"fgxkcvkqp	2085;	205; 3	20673	20343	2054:	20368
Eqghhkekgpv"qh"Xctkcvkqp" ' "	505: 4	40359	502: 3	20: 57	60959	403: 4
Olpkow o	390; 38	390: 65	360293	3604: ;	80649	8076;
Oczkow o	3;0: :4	3:0983	370799	360922	906: 9	80; 8:
Pwodgt"qh"Urgekogpu	39	7	43	:	3;	:
RESULTS	FAIL		PASS		PASS	
Olpkow o"Ceegrvc dng"Gs wx0"Uc o r ng"O gcp	3:055:		360565		808; 5	
Olpkow o"Ceegrvc dng"Gs wx0"Uc o r ng"O lp	39048:		350653		80253	
MOD CV RESULTS	PASS with MOD CV		PASS with MOD CV		PASS with MOD CV	
O q f khkg f"EX" ' "	80222		80222		8058;	
Olpkow o"Ceegrvc dng"Gs wx0"Uc o r ng"O gcp	390; 39		360275		80838	
Olpkow o"Ceegrvc dng"Gs wx0"Uc o r ng"O lp	38023:		340499		70948	

	Qual.	Equiv.	Qual.	Equiv.	Qual.	Equiv.
Fcvc"cu"ogcuwtgf						
Ogcp"Oqfwmwu"*Ouk	20:74	20:69	20957	20948	205:8	20587
Uvcpfctf"fgxkcvkqp	20242	20237	20234	20234	20239	20228
Eqghhkegpv"qh"Xctkcvkqp"'	405:9	30:4;	30886	30873	6057;	30848
Oipkow o	20:42	20:49	20933	20939	2057:	20579
Oczkow o	20::3	20:8:	2097;	20977	20644	20596
Pwodgt"qh"Urgekogpu	43	32	43	:	43	:
RESULTS		PASS		PASS		FAIL
Rcuulp i"Tcpig"hq t"Oqfwmwu"Ogcp	20:59"vq 20:89		20947"vq 20968		20596"vq 205;;	
Uvwfgpvju"v/uvckvke	206899		202092		202074:	
r/xcmwg"qh"Uvwfgpvju"v/uvckvke						
MOD CV RESULTS		PASS with MOD CV		PASS with MOD CV		FAIL
Oqfhhkf"EX'	20:3:"vq"20::8		20925"vq"2098:		2058:"vq"20626	
Rcuulp i"Tcpig"hq t"Oqfwmwu"Ogcp	/20562		/20782		/40737	
r/xcmwg"qh"Uvwfgpvju"v/uvckvke	20958		207:2		2023:	

Hkiwtg"5/: "knnwuvtcvgu"vjg"KRU"uvtgpi vj" o gcpu"cpf" o kpk o w o "xcnwgu"cpf"vjg" o qfwnwu" o gcpu"hqt"vjg" swcnkhkecvkqp"uc o rng"cpf"vjg"gs wxcngpe{ "uc o rng0"Vjg"nk o kvu"hqt"gs wxcngpe{ "uc o rngu"ctg"ujqyp" cu"gttqt"dctu"ykvj"vjg"swcnkhkecvkqp"fcvc0"Vjg"nqpi gt."nki jvgt"eqnqtgf"gttqt"dctu"ctg"hqt"vjg" o qfkhkgf"EX"eq o rwvcvkqpu0"

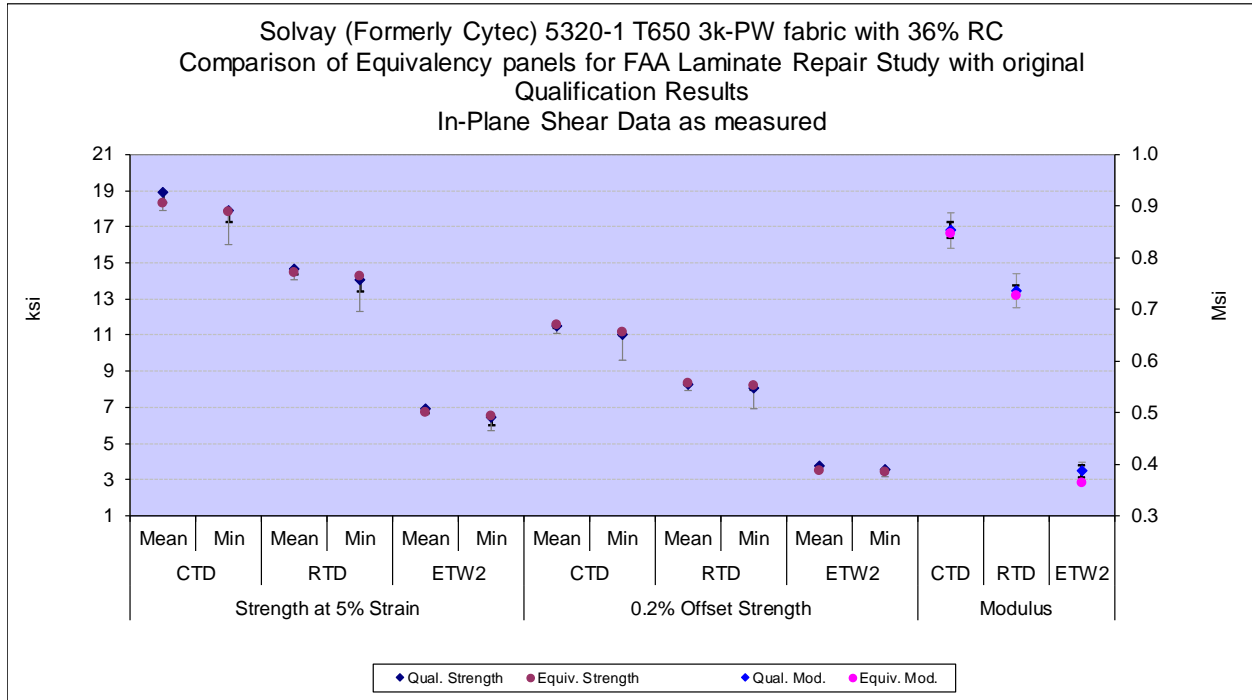


Figure 3-8 In-Plane Shear means, minimums and Equivalence limits

3.7 “25/50/25” Open Hole Tension 1 (OHT1)

Vjg"QJV3"fcvc"ku"pqt o cnk |gf0"Vjg"QJV3"uvtgpi vj"fcvc"rcuugf"gs wxcngpe{"vguvu"hqt"cn"vguvgf"
 eqpfkvkqpu0""Uvcvkuvkeu"cpf"cpn{uku"tguwnvu"hqt"vjg"QJV3"uvtgpi vj"fcvc"ctg"ujqyp"kp"Vcdng"5/370"
 "

	Qual.	Equiv.	Qual.	Equiv.
Fcvc"pqt ocnk gf"ykvj"ERV"202299				
Ogcp"Uvtgpi vj"*muk+	650867	650;73	6:0856	6:02:;
Uvcpfctf"Fgxkcvkqp	50564	30;65	3088;	3062:
Eqghhkekgpv"qh"Xctkcvkqp"'	90879	60642	50654	40;4;
Oqpkowo	590:99	620772	680257	680379
Oczkowo	6;08:9	6807;2	750438	6;0966
Pwodgt"qh"Urgekogpu	3;	:	3;	:

RESULTS

3.9 “25/50/25” Compression After Impact 1 (CAI1)

Vjg"ECK3"fcvc"ku"pqt o cnk | gf0"Vjg"ECK3"uvtgpi vj"fcvc"rcuugf"gs wxcngpe{"vguvu"hqt"vjg"TVF"
eqpfkvkqp"dww"jcu"kpwwhhkekgy"fcvc"hqt"vjg"tguwnvu"vq"dg"eqpukfgtgf"eqpenwukxg0""Uvcvkuvkeu"cpf"
cpcn{ r 2 O o O O ssgC O vg O O _ O

3.10 Cured Ply Thickness (CPT)

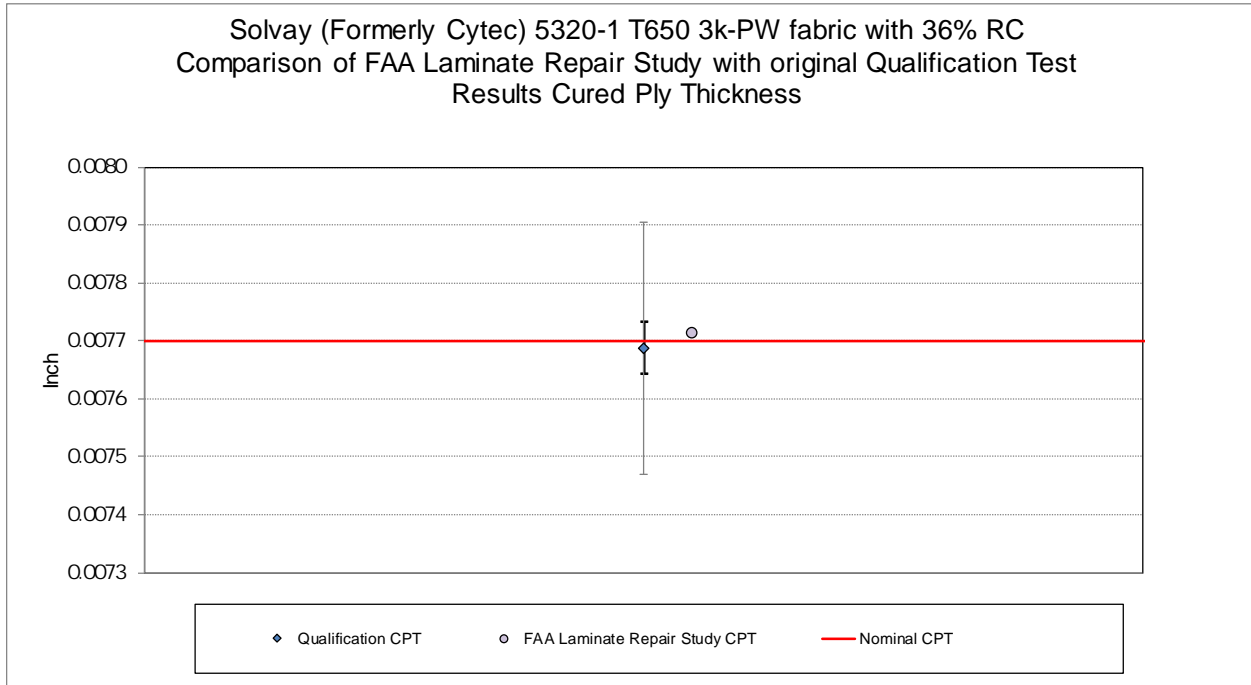


Figure 3-12 CPT means, 95% standard error bars and nominal value

3.11 Dynamic Mechanical Analysis (DMA)

FOC"ku"eq o rctgf"hqt"v yq" o gcuwtg o gpvu."v jg"qpugv"qh"uvqtci g" o qfwnwu"cpf"v jg"rgcm"qh"vcpi gpv"
fgnvc"hqt"dqv j"ft{"cpf"y gv"eqpfkvkqpu0"V jgug"ctg"vguvvf"hqt"gswxengpe{"wukpi"c"rqngf"v yq/
uc o rng"fqwdng/ukfgf"v/vguv"cv"c";7 "'eqphkfgpeg"ngxgm0"V jg"o qfkhkgf"EX"o gvjqf"ku"pqv"cr rnkf"vq"
FOC."dwy"cp"cf fkvkqpcn"cpnc{uku"ku"cnuq"o c f g"y kvj"v jg"cnny cdng"tcpig"hqt"FOC"dgkpi"ugv"vq"
Õ3: ÅH0"V jku"gswxengpe{"etkvgtkqp"hqt"gxcnwcvkpi"i ncuu"vtcpukvqp"vg o rgtcvwtg"ku"pqv"c"uvcvkuvkecnn{/
dcugf"etkvgtkqp"dwy"ku"i gpgtcnn{"o qtg"uvtkpi gpv"v jcp"v jcv"dcugf"qp" ?7 "'y kvj"o qfkhkgf"eqghhkegpv"
qh"xctkcvkqp"dwy"nguu"uvtkpi gpv"v jcv"v jcv"dcugf"qp" ?7 "'y kvj"cu/o gcuwtgf"eqghhkegpv"qh"xctkcvkqp0"
V jku"etkvgtkqp"ku"cf f g f"vq"v jg"vguv"qp"V i"vq"ckf"v jg"fgekukqp"o cmkpi"rtqegu"dgecwug"v jg"
uvcvkuvkecnn{/dcugf"o gvjqfu"ctg"qhvqp"vqq"uvtkpi gpv"*y jgp"cu/o gcuwtgf"eqghhkegpv"qh"xctkcvkqp"ku"
wugf+"qt"vqq"ncz"*y jgp"o qfkhkgf"eqghhkegpv"qh"xctkcvkqp"ku"wugf+0"

V jg"FOC"ft{"fcvc"ugvu"y gtg"unk i j vn{"cdq xg"v jg"wr rgt"ceegrvcpeg"nk o kvu"y jkng"v jg"FOC"y gv"fcvc"
ugvu"y gtg"unk i j vn{"dgnqy"v jg"nq y gt"ceegrvcpeg"nk o kvu0""J qy g xgt."v jg"FOC"fcvc"rcuugf"
gswxengpe{"vguvu"hqt"dqv j"v jg"ft{"Rgcm"qh"Vcpi gpv"FGnvc"cpf"v j

"

Vjg"Rgcm"qh"Vcpi gpv" Fgnvc"hqt" ygv" fcvc"hckngf"vjg"gswkxcngpe{"vguv"dgecwug"vjg"uc o rng" o gcp"
xcnwg"*5630722+"ku"dgnqy"vjg"nqygt"ceegrvcpeg"nk o kv"*5640:48+0"Vjg"gswkxcngpe{"uc o rng" o gcp"ku"
; ;083 ' "qh"vjg"nqygt"nk o kv"qh"ceegrvcng"xcnwg"Ykvj"vjg"cnqy cdng"tcpig"ugv"vq"Ô3: ÅH."vjg"Rgcm"
qh"Vcpi gpv" Fgnvc"hqt"FOC" ygv"fcvc"rcuugf"vjg"gswkxcngpe{"vguv0"

"

Hkiwtg"5/35"knwuvtcvgu"vjg"cxgtcig"Vi"xcnwg"fgvgt okpgf"htqo"FOC"hqt"dqvj"vjg"swcnkhkecvkqp"
uc o rng"cpf"vjg"gswkxcngpe{"uc o rng0"Vjg"nk o kvu"hqt"gswkxcngpe{"uc o rngu"ctg"ujqyp"cu"gttqt"dctu"
ykvj"vjg"swcnkhkecvkqp"fcvc0"Vjg

4. Summary of Results

Cm"vjg"gswxncngpe{"eq o rctkuqpu"ctg"eqpfwevgf"ykvj"V{ rg"K"gttqt"rtqdcdknv{"* +"qh"7 ' "kp"
ceeqtfcpeg"ykvj"HCC1FQVICT/2513;"tgrqtv"cpf"EO J /39/3 I"ugevkqp":06030"kv"ku"eq o o qp"vq"
qdvckp"c"hg y"qt"gxgp"ugxgtcn"hcknwtgu"kp"c"v{ rkecn"gswxncngpe{"rtqi tc o"kpqxnxkpi" o wnwkrng"
kpfgrgpfgp"rtqrgtv{"eq o rctkuqpu

4.2 Failures

Vjg"HCC"Nc o kpcvg"Tr rckt"Uvwf { " o cvgtkc n" j cu"uw h h k e k g p v"v g u v"t g u w n v u" h q t" e q o r c t k u q p" y k v j" v j g"
q t k i k p c n" s w e n k h k e c v k q p" o c v g t k c n" v g u v" t g u w n v u" q p" c" v q v c n" q h" 5 ; " f k h h g t g p v" v g u v" v { r g u" c p f" e q p f k v k q p u. " p q v"
k p e n w f k p i" v j g" e w t g f" r n { " v j k e m p g u u" q t" v j g" F O C" e q o r c t k u q p 0"
"

Wukpi"vjg" o q f k h k g f"EX" o g v j q f."v j g t g" y g t g" v y q" h c k n w t g u 0" D q v j" h c k n w t g u" y g t g" h q t" K R U" r t q r g t v k g u"
*204 ' " q h h u g v" u v t g p i v j" c p f" o q f w n w u+ " k p" v j g" G V Y 4" e q p f k v k q p 0"
"

- 30 Kp/Rncpg"Ujgct"Oqfwnwu"hqt"vjg"GVY4"eqpfkvkqp"hckngf"d{"302: ' ' "
- 40 Kp/Rncpg"Ujgct"204 ' "Qhhugv"Uvtgp

4.4 Probability of Failures

Kh"vjg"gswxncngpe{"uc o rng"ec o g"htq o "c" o cvgtken"ykvj"ejctcevgtkuvkeu"kfgpvkecn"vq"vjg"qtki kpcn" swcnkhkecvkqp" o cvgtken"cpf"cnm"vguvu" ygtg"kpfgrgpfgpv"qh"cnm"qvjgt"vguvu."vjg"ejcpeg"qh"jcxkpi"vyq" qt" o qtg"hcknwtgu"ku"7:093 ' 0"Hkiwtg"6/3"knwuvvcygu"vjg"rtqdcdknkv{"qh"igvvpki"qpg"qt" o qtg"hcknwtgu." vyq"qt" o qtg"hcknwtgu."gve0"htq" c"ugv"qh"5;"kpfgrgpfgpv"vguvu0"Kh"vjg"vyq" o cvgtken" ygtg"gswxncngpv." vjg"rtqdcdknkv{"qh"igvvpki"hxg"qt" o qtg"hcknwtgu"ku"nguu"vjcp"7 ' 0"Vjku" o gcpu"vjcv"vjg" o cvgtken"eqwnf" dg"eqpukfgtgf"cu"öpqv"gswxncngpvö"ykvj" c";7 ' "ngxgn"qh"eqphkfgpeg"kh"vjgtg" ygtg"hxg"qt" o qtg" hcknwtgu"qvv"qh"5;"kpfgrgpfgpv"vguvu0"

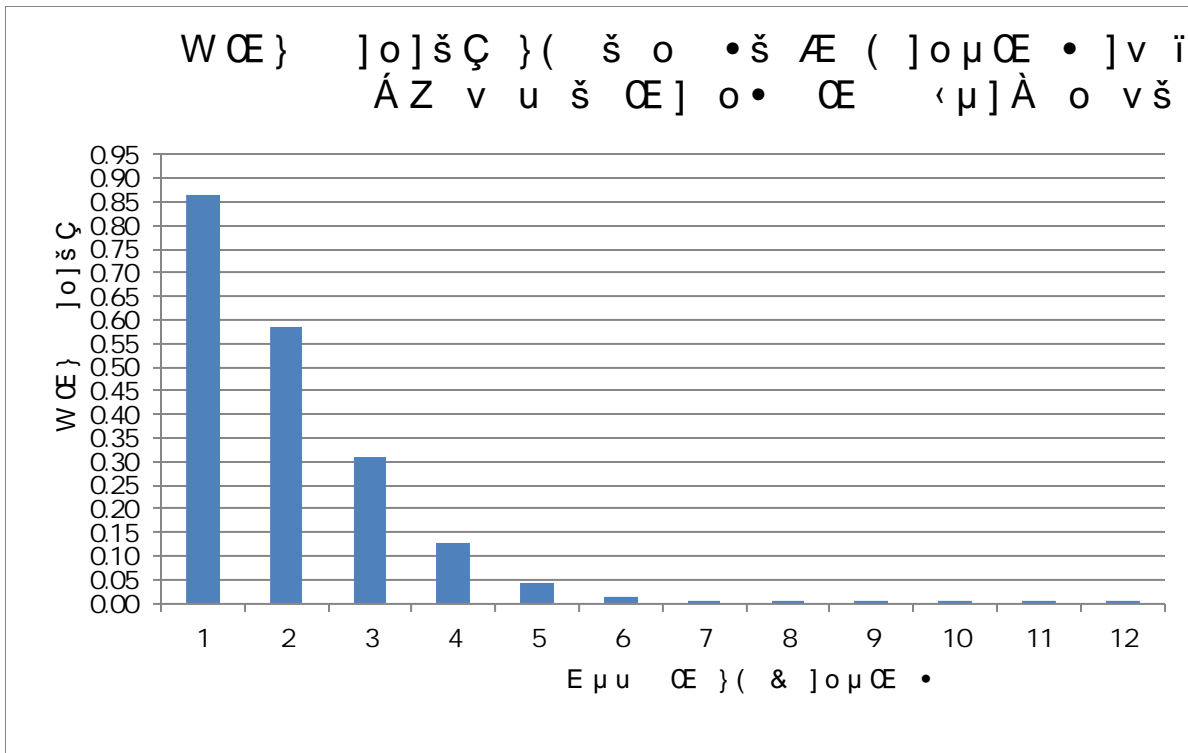


Figure 4-1 Probability of Number of Failures

5. References

- 30 EO J/39"Tgx" I."Xqnw o g"3."42340"UCG"Kpvgtpcvkqpcn."622"Eq o o qpy gcnvj" Ftkxg." Ycttgpfng."RC"372;8"
- 40 Lqjp"Vq o dnpk." [gqy "E0"Pi."cpf"M0"Uwtguj" Tclw."öMaterial Qualification and Equivalency for polymer Matrix Composite Material Systems: Updated Procedureö." Pcvkqpcn"Vgejpkecn"Kphqt o cvkqp"Ugtxkeg"*PVKU+."Urtkpi hkgnf."Xkti kpkc"44383"
- 50 Xcpi gn."Octm."\$Nqv"Ceegrvcpeg"cpf"Eq o rnkcepg"Vguvkpi" Wukpi"vjg"Uc o rng"Ogcp"cpf" cp"Gzvtg o w o \$."Vgejppq o gvtkeu."Xqn"66."PQ0"5."Cwiwuv"4224."rr0"464/46;"